

Power Loss Reduction and Voltage Profile Improvement in Electrical Power Distribution Networks Using Static Var Compensators

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Abstract—Rising demand for electrical power due to the global technological advancement has brought so many challenges such as instability of voltage, huge power loss, and unstable power factor on the distribution network. This work applied Static Var Compensator (SVC) to the power distribution network of Ado-Ekiti, Nigeria, to study its effect on active power loss reduction and voltage profile improvement of the network. The bus voltage, power, and the current flowing through the selected feeders were measured and recorded accordingly for analysis. Test network parameters like route length, transformer parameters, and maximum power flow were obtained from Benin Electricity Distribution Company, Ado-Ekiti, Nigeria. The distribution network was then modeled and simulated with and without SVC in NEPLAN software environment. The simulation results of the power flow and voltage stability analyses of the network without SVCs showed that some distribution lines were overloaded and that the network parameters were not within the statutory tolerable limits of 0.95 p.u. and 1.05 p.u. nominal voltage. There was 9.73% reduction in the active power loss when SVCs were incorporated into the test network. The voltage stability curve showed an increase in distribution network capacity from an initial steady-state of 150% to 263% of the total active load when the SVCs were incorporated. Hence, the need to normalize the network by applying SVCs to all the buses with very low voltages. This work will assist the power distribution supply companies in making some informed decisions in reducing power losses on their networks.

Keywords— Active power loss; distribution network; NEPLAN; static var compensator; voltage fluctuation.

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I. INTRODUCTION

Electrical power is an inherent commodity because it drives the economy and sustains the developmental growth of any country. There is, therefore, an interrelation between the standard of living and the available power delivered in a country [1], [2]. Electricity distribution systems deal with collecting activities and equipment to ensure that power is effectively delivered from the transmission station to the final electricity end-users [3], [4].

In electrical power distribution networks, network power loss and voltage stability are the most important factors showing the quality of power supplied to the electricity end-users [5]. Electrical and electronic devices are designed to work on a specified voltage, frequency, and current rating. Variation from the specified values discomposes weighty menaces to the whole power networks [6].

The power distribution network in Nigeria is peculiar with heavy power losses and voltage drop, which is a major cause of very poor quality of electrical power arriving at electricity

end-users [7]. Electrical power network suffers largely from voltage instability especially due to excessive consumption or injection of reactive power by the system elements and the consumers' load. The network's voltage goes high if there is the excessive injection of reactive power by the network elements or the electricity end-user's loads but goes low if the reactive power being consumed by the network elements or electrical load is excessive.

As a result, the power system's reactive power needs to be constantly regulated through adequate reactive power compensation [5]. In this case, the old-fashioned techniques employed include reconfiguring network structure, synchronous generator, changing the voltage by transformer tap to regulate the power flow in the grid, and series compensation capacitors [8]. With these techniques, the desired objectives were not efficiently realized, with wear and tear in mechanical devices and slow response being the main challenges [9].

The existing distribution line basic facility is not capable of supporting the increasing load demand. These result in

voltage drop profile, increased network losses, poor network efficiency, instability, and disturbance [10]. Under the pressured situation, one of the efficient ways to save the network from voltage collapse is to lessen the reactive power load or add additional reactive power sources by introducing reactive power sources such as Static Var Compensator (SVC) [11]. The SVC has a positive contact on improving the network voltage profile, improving the power factor, voltage stability, and minimizing power loss. According to the Institute of Electrical and Electronics Engineers (IEEE), the allowable voltage standard is between 0.95 p.u. and 1.05 p.u. [12]. A suitable electric power network must have a voltage that does not exceed the tolerance limit and have very small power losses. The voltage drop affects the power losses. Power losses are inevitable but can be minimized by enhancing the voltage profile.

Extensive research works were carried out recently, leading to the discovery of Flexible AC transmission system (FACTS) devices that have been chiefly employed to solve different power system steady-state control problems such as power flow control, voltage regulation, and transferability improvement near-instantaneous response [13]. Many studies [3], [19] have shown that most of the electrical power quality issues directly result from deviations in the network's reactive power. FACTS technology that shows the rapid response to network changes was used by Beagon *et al.* [14] to enhance power network efficiency without changing the network structure. Singh and Agrawal [10] worked on improving voltage profiles by reducing the active and reactive power losses using optimal load flow methodology in MATLAB environment. This was done by the incorporation of SVC in the power system network. The effectiveness of the methodology was tested on IEEE-9 and IEEE-30 bus systems.

Jumat *et al.* [11] modeled and simulated SVC using MATLAB/Simulink software to improve the voltage profile of a transmission system. The proposed methodology was validated using four case study areas. The simulation results showed a positive effect on the system's voltage. An optimal location and number of Unified Flow Controller (UPFC) devices to improve voltage profile and reduce the electrical system losses were carried out by Hocine and Djamel [13]. The work proposed a method by which the optimal number, size, and locations of UPFC enhance reduced system losses and enhance voltage profile. The methodology was applied to a standard IEEE 14 test system. Suliman [20] worked on voltage profile improvement on the distribution network. The work presented a fuzzy controller based on Static Synchronous Compensator (STATCOM). The stability margin was increased by about 20%.

Most of the research reviewed so far used different loss minimization techniques that get more complicated as the number of buses increases. The methods adopted also depend on the specific case study areas. It can be observed that most of the work done was on voltage improvement and loss reduction on transmission networks. However, this paper seeks to study the effect of SVC in reducing the network's active power loss and improving voltage profile through adequate reactive power compensation using an electrical power distribution network, Ado-Ekiti, Nigeria, as a test system.

A. Power Flow Analysis

Load flow analysis is a suitable tool to ascertain the complex electrical power system [15]. It is used to evaluate reactive and active power and voltage and electric current passing through the power line at different buses in a network. It is also helpful for effective planning and monitoring of network's behavior and evaluating the best size and suitable location of shunt devices to improve the power factor, voltage level and minimize the network power loss.

B. The Flexible AC Transmission System (FACTS) Controllers

FACTS controllers are used to improving the controllability and raise the electrical power transferability of a distribution network. There are several types of FACTS controller configuration, such as Thyristor-controlled phase shifter (TCPS), Static Synchronous Series Compensator (SSSC), Thyristor-controlled series compensator (TCSC), Static Synchronous Compensator (STATCOM), and Static Var Compensator (SVC) [16]. The FACTS controller considered in this work is SVC because it is reliable and not expensive. A Static Var Compensator (SVC) is a parallel combination of a controlled reactor and switched capacitor. It is used to supply rapid operating reactive power in the electrical power network. It combined both capacitors and reactors for rapid regulation of electrical power network variables [17]. They are applied in electrical power networks for various purposes, the principal of which is fast control of bus voltage at weak buses in an electrical power network. Static Var Compensator-TCR-TSC is shown in Figure 1.

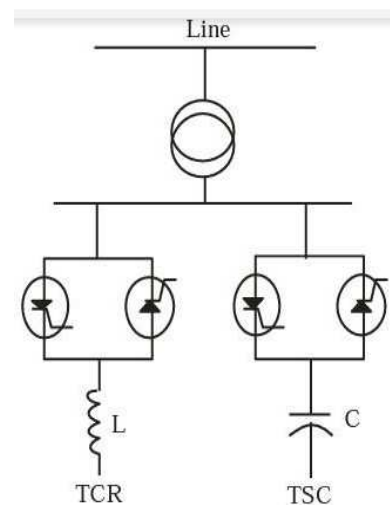


Fig. 1 Static var compensator-TCR- TSC [15]

Majorly, SVC comprises a fast thyristor switch regulating both shunt capacitor and inductor [17], [21]. SVC is connected as thyristor-controlled-reactor and thyristor-switched capacitor (TCR-TSC). The term "Static" is used to show that SVC has no rotating main components. The thyristor switch assembly regulates the voltage across the inductor and, therefore, the electric current flowing through the inductor. Thus, the reactive power absorbed by the inductor can be regulated [19], [20], [23].

II. MATERIALS AND METHODS

The test distribution network considered for this study is the 33/11 kV injection substation, Ado-Ekiti, Nigeria. The single line diagram of the substation network is as shown in Figure 2. The substation consists of two power transformers, each having capacity of 15 MVA. There are two outgoing feeders connected to each of the power transformers, the incoming voltage level is 33 kV, and the distribution voltage level is 11 kV. The electrical loads connected to the output terminals of the distribution transformer receive a voltage of 0.415 kV. For the simplicity of the network analysis, the total distribution transformers on each feeder are shown by its equivalent single distribution transformer.

The two selected feeders (Adebayo and Okesa) were considered for the analysis.

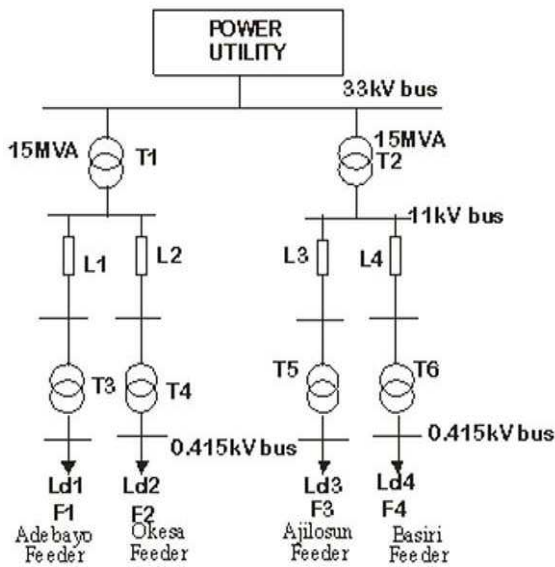


Fig. 2 Single line diagram of the 33/11 kV injection substation, Ado-Ekiti

The selected network data such as total route length of the distribution feeders, distribution transformer parameters, active and reactive power sent, bus voltage, and system power factor needed for the load flow analysis were obtained from Benin Electricity Distribution Company's records Nigeria (BEDC). The relevant data for the 33/11kV Injection substation is as in Table 1, Table 2, and Table 3. The load current at each load point was measured and recorded accordingly (Appendices A and B) at peak load conditions. This was used in estimating the total load demand on each of the distribution transformers.

TABLE I
RELEVANT RECORDED DATA OF THE 33/11 KV POWER NETWORK,
ADO-EKITI

11 kV Feeders	Active power sent (MW)	Reactive power sent (MVAR)	Bus Voltage (kV)	Power Factor (P.F)	Current (A) at Feeders
Adebayo	6.30	2.29	110.8	0.94	360
Okesa	5.10	2.01	110.9	0.93	288
Basiri	6.02	2.07	111.0	0.95	346
Ajilosun	5.85	2.00	111.0	0.95	334

TABLE II
DISTRIBUTION LINE PARAMETERS

Parameter	Adebayo Feeder	Okesa Feeder
Resistance per km in ohm	0.28	0.28
Reactance per km in ohm	0.32	0.32
Route length in km	28.7	13.8

TABLE III
TRANSFORMERS ON EACH FEEDER

11 kV Feeders	500 kVA	315 kVA	300 kVA	200 kVA	TOTAL L
Adebayo	13	1	19	2	35
Okesa	9	1	14	1	25

A. Mathematical Model of Distribution Network

The network can be represented by an equivalent single-line diagram in a balanced distribution system, as shown in Figure 3. The line shunt capacitances at distribution voltage levels are very small and, therefore, can be neglected [21], [23]. The mathematical model of the radial distribution network is derived from Figure 3. Equation 1 and Equation 2 were derived as expressed in Figure 3.

$$I_{(jj)} = \frac{V_{(m_1)} \angle \delta_{(m_1)} - V_{(m_2)} \angle \delta_{(m_2)}}{Z_{(jj)}} \quad (1)$$

$$P_{(m_2)} - jQ_{(m_2)} = V_{(m_2)} \times I_{(jj)} \quad (2)$$

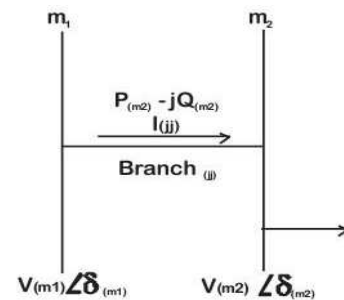


Fig. 3 Mathematical model of distribution network [21]

where,

m_1 and m_2 are the sending and receiving end buses respectively,

$P_{(m_2)}$ is the addition of active power loads of all the buses beyond bus m_2 plus active power load of the bus m_2 itself plus the addition of the active power losses of all the branches beyond bus m_2 ,

$Q_{(m_2)}$ is the addition of reactive power loads of all the buses beyond bus m_2 plus reactive power load of the bus m_2 itself plus the addition of the reactive power losses of all the branches beyond bus m_2 ,

$I_{(jj)}$ is the current flowing through the branch jj ,

$V_{(i)}$ is the magnitude of the voltage of the i^{th} node,

$\delta_{(m_1)}$ is the voltage angle of node m_1 ,

$\delta_{(m_2)}$ is the voltage angle of node m_2 ,

$R_{(jj)}$ is the resistance of the branch jj ,

$X_{(jj)}$ is the reactance of the branch jj .

From Equation 1 and Equation 2, we get Equation 3

$$V_{(m_2)} = \sqrt{B_{(jj)} - A_{(jj)}} \quad (3)$$

where,

$$A(jj) = P(m2) \times R(jj) + Q(m2) \times X(jj) - 0.5 \times [V(m1)]^2 \quad (4)$$

$$B(jj) = \sqrt{A^2(jj) - [Z^2(jj) \times (P^2(m2) + Q^2(m2))]} \quad (5)$$

The real and reactive power loss of branch jj is given by Eq.6 and Eq.7

$$LP(jj) = \frac{R(jj) \times [P^2(m2) + Q^2(m2)]}{V(m2)^2} \quad (6)$$

$$LQ(jj) = \frac{X(jj) \times [P^2(m2) + Q^2(m2)]}{V(m2)^2} \quad (7)$$

Calculations were performed successively till the convergence standard is obtained [21], [22], [24], [25].

B. Research Approach

This detailed modeling and simulation of the 11 kV distribution network, Ado-Ekiti by supplying the data obtained into advanced computer aided analysis tool (NEPLAN software). The systematic flowchart for the research is as shown in Figure 4.

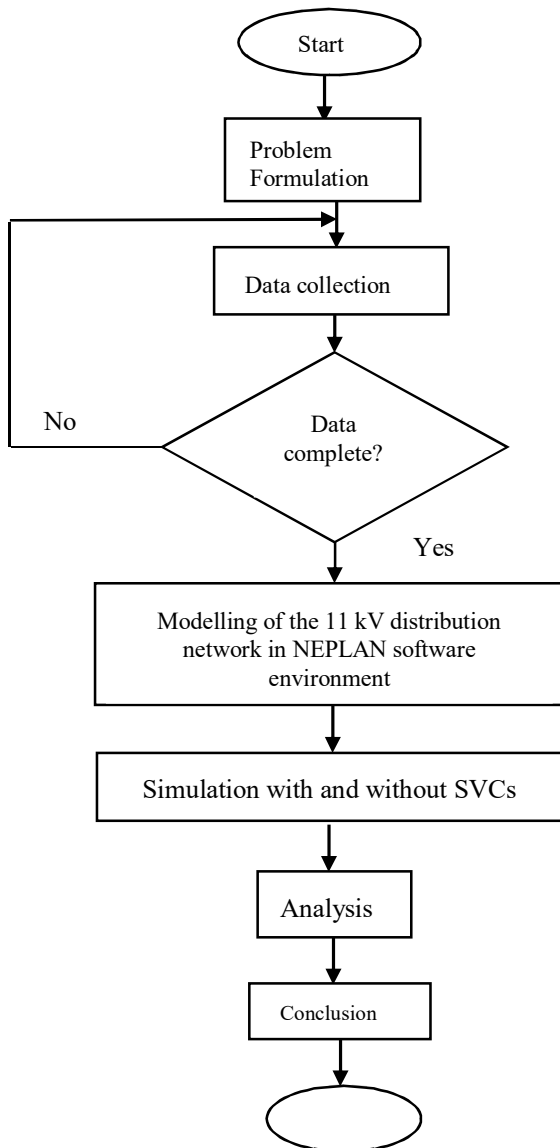


Fig. 4 Systematic flowchart for the research methodology

The distribution network (Figure 2) was considered for load flow analysis based on the following assumptions.

- The incoming 33 kV bus is considered as slack or reference assumptions.
- Length of 0.415 kV low tension service line is neglected.
- All loads are assumed to be static.
- The analysis is made for the steady state condition.
- Tolerance limits 0.95 p.u to 1.05 p.u of normal voltage

The distribution network was then modeled with and without FACTS controller (SVC) using NEPLAN software. These were subsequently discussed in the following sub-sections.

1) Simulation without FACTS controllers (SVCs):

Simulation without SVC was carried out. The distribution network (Figure 2) was modeled and simulated in NEPLAN environment. The selected network data was used as inputs to create a virtual diagrammatic simulator, as shown in Figure 5. The simulation is carried out in stages as follows:

- *Step 1:* Selection of components. Power system components like transformers, distributions line, buses, loads are selected from the NEPLAN library.
- *Step 2:* Development of the network: Single line diagram was developed using different elements in the NAPLAN library.
- *Step 3:* Mode for analysis: The Newton Raphson Technique was employed for the network modeling and simulation due to its remarkable convergence.
- *Step 4:* Simulation output: Power flow was carried out, and results were obtained.

2) *Simulation with FACTS Controllers (SVCs):* Simulation with controllers is carried out using the steps explained in subsection 1 in the previous section. SVCs are applied to weak buses, and the computer simulation is done on the selected network in order to obtain results based on the input data.

III. RESULTS AND DISCUSSIONS

The results of the simulation as carried out in the previous section are presented and discussed in this section.

A. Simulation Results with and without FACTs Controllers (SVCs)

The power flow analysis results of the 11 kV-bus voltages (Adebayo feeder) with and without SVCs are shown in Figure 6, while the load bus voltage (Adebayo feeder) with and without SVCs is as in Table 4. The power flow analysis results of the 11 kV-bus voltages (Okesa feeder) with and without SVCs are shown in Figure 7, while the load bus voltage (Okesa feeder) with and without SVCs is as in Table 5. Figure 8 shows the voltage stability curve obtained under the initial steady-state operation without the SVCs, while the voltage stability curve obtained after normalizing (with SVCs) the network operating parameters are shown in Figure 9. The total active power loss with and without SVCs is as shown in Figure 10.

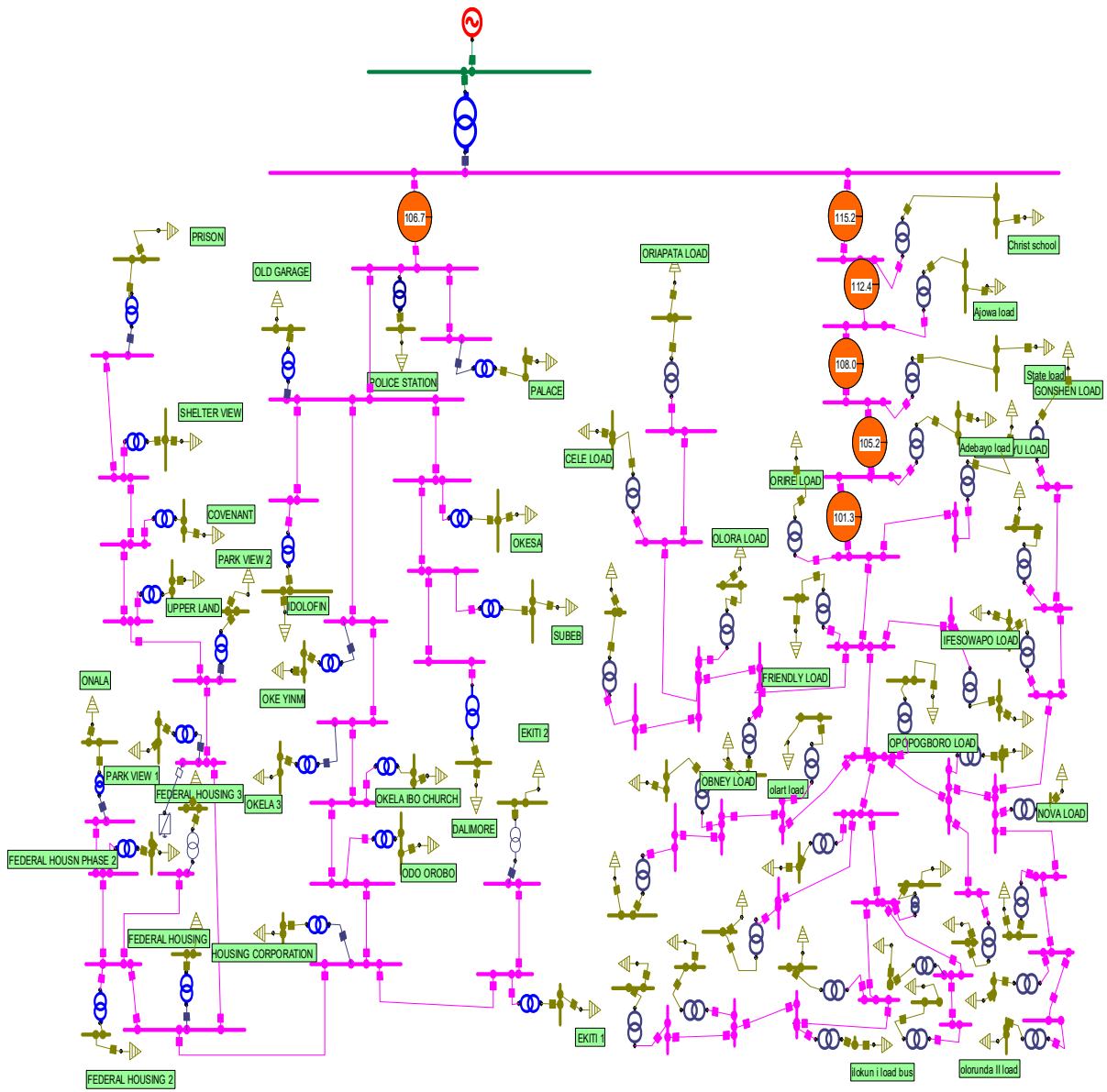


Fig. 5 The modelled-Ado-Ekiti 33/11 kV power network in NEPLAN without SVCs

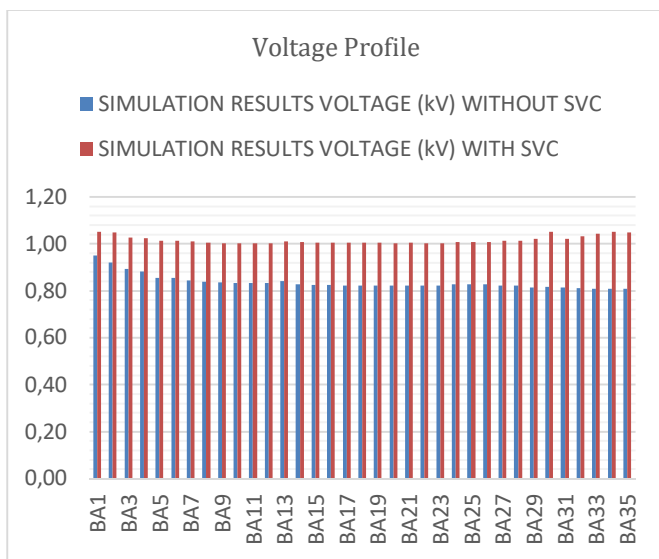


Fig. 6 Voltage profile of 11 kV (Adebayo) feeder with and without SVCs

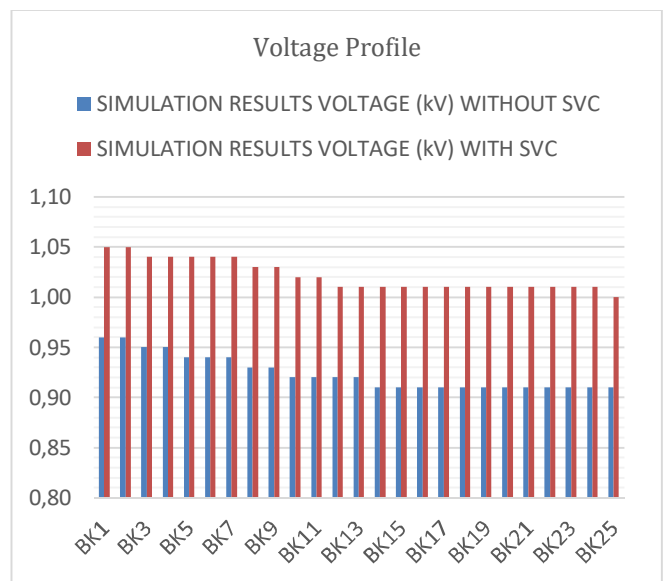


Fig. 7 Voltage profile of 11 kV (Okesa) feeder with and without SVCs

TABLE IV
LOAD BUS VOLTAGES (ADEBAYO FEEDER) WITHOUT AND WITH SVCS

Bus No	Load Bus Name	Simulation Results Voltage (kV)			
		Without SVC		With SVC	
		(kV)	V(p.u.)	(kV)	V(p.u.)
1	Christ School	0.388	0.935	0.431	1.039
2	Ajowa	0.377	0.908	0.426	1.027
3	State	0.367	0.884	0.423	1.019
4	Adebayo	0.361	0.87	0.42	1.012
5	Orire	0.35	0.843	0.416	1.002
6	Jimoh Aliyu	0.35	0.843	0.417	1.005
7	Friendly	0.343	0.827	0.414	0.998
8	Obey	0.341	0.822	0.412	0.993
9	Olora	0.336	0.81	0.408	0.983
10	Ifelore	0.341	0.822	0.412	0.993
11	Cele	0.34	0.819	0.411	0.99
12	Oriapata	0.34	0.819	0.411	0.99
13	Iyalaje	0.345	0.831	0.415	1
14	Opopogbooro	0.338	0.814	0.414	0.998
15	Abaibira 1	0.338	0.814	0.414	0.998
16	Abaibira 1	0.339	0.817	0.414	0.998
17	Nova	0.335	0.807	0.411	0.99
18	Ifesowapo	0.336	0.81	0.412	0.993
19	Aponwe	0.337	0.812	0.413	0.995
20	Goshen	0.336	0.81	0.413	0.995
21	Olorunsogo	0.329	0.793	0.407	0.981
22	Olorunda 1	0.334	0.805	0.411	0.99
23	Olorunda 2	0.335	0.807	0.412	0.993
24	Olarat	0.338	0.814	0.414	0.998
25	Balemo	0.336	0.81	0.413	0.995
26	Bolorunduro	0.338	0.814	0.414	0.998
27	Adehun	0.336	0.81	0.417	1.005
28	Ileileri	0.33	0.795	0.412	0.993
29	Peace 1	0.334	0.805	0.421	1.014
30	Peace 2	0.335	0.807	0.421	1.014
31	Ore Ofè	0.332	0.8	0.42	1.012
32	Irewumi	0.333	0.802	0.425	1.024
33	Ilokun 1	0.295	0.711	0.407	0.981
34	Ilokun 2	0.331	0.798	0.43	1.036
35	Isegere	0.35	0.795	0.432	1.041

TABLE V
LOAD BUS VOLTAGE (OKESA FEEDER) WITHOUT AND WITH SVCS

Bus No	Load Bus Name	Simulation Results Voltage (kV)			
		Without SVC		With SVC	
		(kV)	V(p.u.)	(kV)	V(p.u.)
1	Police Station	0.392	0.94	0.43	1.04
2	Palace	0.389	0.94	0.427	1.03
3	Old Garage	0.386	0.93	0.425	1.02
4	Idolofin	0.382	0.92	0.421	1.01
5	Oke-Ese	0.389	0.94	0.427	1.03
6	SUBEB	0.386	0.93	0.425	1.02
7	Dallimore	0.384	0.93	0.423	1.02
8	Okeyinmi	0.384	0.93	0.423	1.02
9	Okeila 3 (Rosebud)	0.381	0.92	0.42	1.01
10	Oke ila (Ibo Church)	0.379	0.91	0.419	1.01
11	Odo Orobo	0.375	0.90	0.415	1.00
12	Housing Corporation	0.375	0.90	0.415	1.00
13	Ekiti 1	0.378	0.91	0.417	1.00
14	Ekiti 2	0.38	0.92	0.419	1.01
15	Fed. Housing 1	0.37	0.89	0.41	0.99
16	Fed. Housing 2	0.37	0.89	0.41	0.99
17	Fed housing 3	0.374	0.90	0.414	1.00
18	Fed Housing Phase 2	0.374	0.90	0.414	1.00
19	Onala	0.372	0.90	0.412	0.99
20	Park view 1	0.371	0.89	0.411	0.99
21	Park View 2	0.372	0.90	0.412	0.99
22	Upper Load	0.373	0.90	0.413	1.00
23	Covenant	0.37	0.89	0.41	0.99
24	Shelter View	0.374	0.90	0.415	1.00
25	Prison	0.375	0.90	0.415	1.00

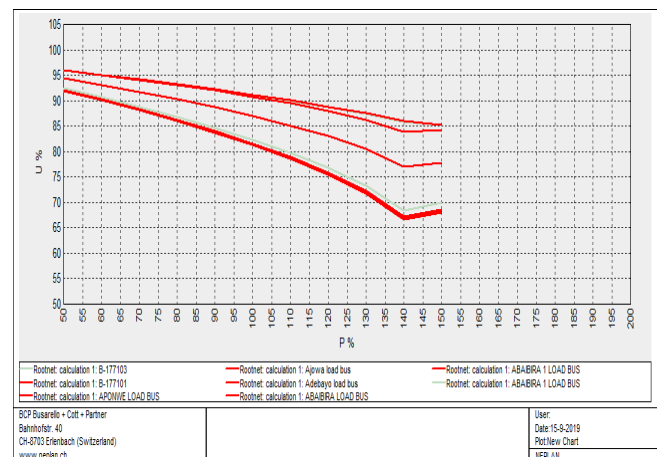


Fig. 8 Voltage stability curve under initial steady state operation without SVCs

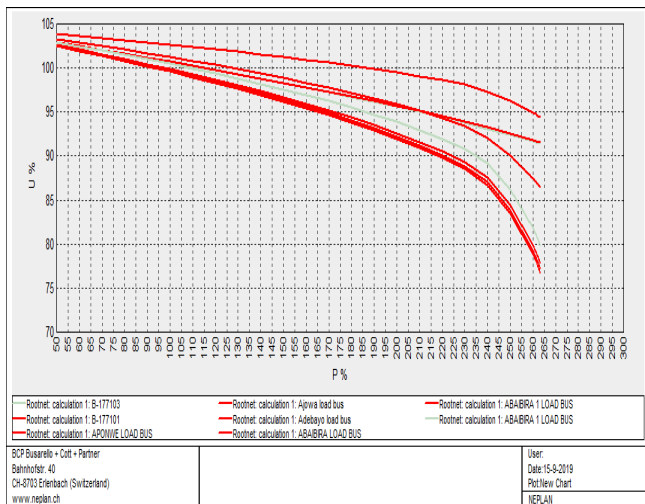


Fig. 9 Voltage stability curve under normal steady-state operation with SVCs

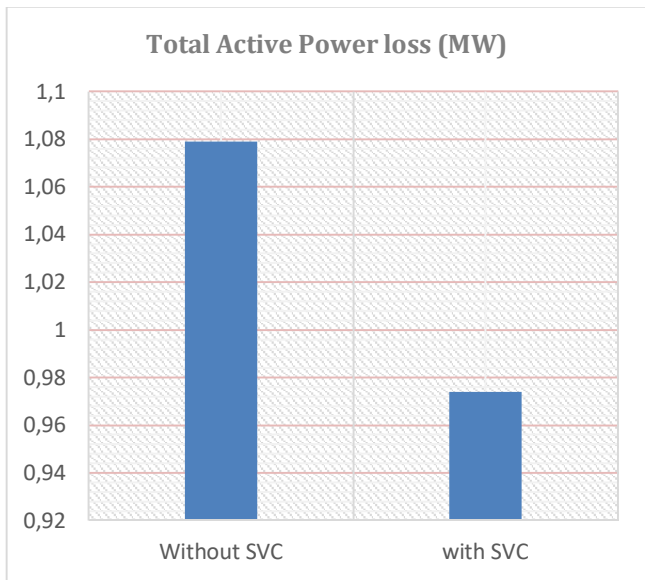


Fig. 10 Total active power loss with and without SVCs

B. Discussion

The simulation results with and without SVCs were discussed in the following subsections.

1) *Simulation without FACTs controllers (SVCs):* The results show that the network parameters are not within the statutory tolerable limits of 0.95 p.u. to 1.05 p.u. of the nominal voltage when the networks were run without SVCs during peak load conditions, as shown in Table 4, Table 5, Figure 6 and Figure 7. The simulation results of the power flow and voltage stability analysis of the 60-bus network without FACTs controllers shows that some distribution lines are overloaded, the heavily loaded distribution lines and their percentage loading are; Christ School (115.19%), Ajowa (112.4%), State (108.01%), Police Station (106.69%), Adebayo (105.21%) and Orire (101.31%) as in Table IV.

The curve in Figure 9 is a graphical representation of the responses of the bus voltage magnitudes to the increasing values of active loads. The curve also indicates that the maximum transfer capacity of the distribution network under

the initial steady-state stood at 150% of the total distribution network active load.

2) *Simulation with FACTs controllers (SVCs):* The voltage profile of the selected network improved considerably can be observed in Figures 6, Table 4, Figure 7, and Table 5 with the incorporation of SVCs. The voltage stability curve (as in Figure 9), obtained after normalizing the network operating parameters, showed that the distribution network transfer capacity increased to 263% of the total network active load. In order to realize normal line loading of the distribution network, the following requirements were established. Firstly, there is a need to increase the size of the conductor used for the network and normalize various bus voltage magnitudes that have very low values by applying voltage controlling Static Var Compensators.

In order to appreciate the overall effect of FACTs controllers on the distribution networks, it is highly essential to compare the power system's active power loss with and without FACT'S controllers. Figure 10 indicates that the test power network losses stood at 1.079 MW when the network was run without FACT'S controllers and 0.974 MW when run with FACT'S controllers (SVCs). Comparison between the two indicates a 9.73% reduction in total active power loss when FACT'S controllers (SVCs) were incorporated into the test power networks. It can be therefore deduced that SVC application into the distribution network can greatly reduce active power loss.

IV. CONCLUSION

This work applies Static Var Compensator (SVC) to Ado-Ekiti's 11 kV power distribution network, Nigeria. This is to study its effects on active power loss reduction and voltage profile improvement of the network. The distribution network was modeled and simulated in NEPLAN software environment with and without FACT'S controller (SVCs). The simulation results of the power flow and voltage stability analyses of the network without SVCs showed that some distribution lines were overloaded and that the network parameters were not within the statutory tolerable limits. However, with the suitable placement of SVCs, the system bus voltages were enhanced, and the distribution power losses were reduced.

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APPENDIX A
RECORDED DATA FOR 11 KV ADEBAYO FEEDER AT SUBSTATION FOR PEAK LOAD.

S/N	Transformer Name	S/S	Rating (KVA)	Red Phase / (Amp)	Yellow phase / (Amp)	Blue Phase / (Amp)	Neutral (Amp)	Load Current / (Amp)	% Loading
1.	Christ school		300	222	229	218	69	246	59
2.	Ajowa		500	480	295	294	97	389	56
3.	State		500	234	256	219	23	244	35
4.	Adebayo		500	332	326	300	18	325	47
5.	Orire		315	211	217	228	18	225	51
6.	Jimoh aliyu		500	298	288	279	24	296	43
7.	Friendly		300	234	218	219	16	227	54
8.	Obey		200	150	139	147	16	151	54
9.	Oloro		500	623	645	599	23	630	91
10.	Ifelere		300	189	199	200	18	202	48
11.	Cele		500	300	385	335	70	363	52
12.	Oriapata		500	355	315	325	55	350	50
13.	Iyalaje		500	225	247	305	39	272	39
14.	Opopogboro		500	334	325	313	35	336	48
15.	Abaibira 1		300	145	139	142	9	145	35
16.	Abaibira 2		300	145	134	128	8	138	33
17.	Nova		300	235	247	218	31	244	58
18.	Ifesowapo		300	290	162	142	31	175	42
19.	Aponwe		500	234	214	239	17	235	34
20.	Goshen		300	190	162	142	31	392	94
21.	Olorunsogo		300	399	372	369	31	392	94
22.	Olorunda 1		300	234	211	199	46	230	55
23.	Olorunda 2		300	222	198	192	14	209	50
24.	Olart		200	150	120	102	40	137	49
25.	Balemo		300	234	215	241	23	238	57
26.	Bolorunduro		500	252	249	311	40	284	41
27.	Adehun		500	311	276	292	25	301	43
28.	Ileleri		300	358	400	350	40	383	92
29.	Peace 1		500	257	269	301	32	286	41
30.	Peace 2		300	132	122	143	15	137	33
31.	Ore ofe		300	220	205	103	76	207	48
32.	Irewumi		300	125	150	176	30	160	38
33.	Ilokun1		300	148	122	156	31	152	37
34.	Ilokun		300	159	124	149	34	155	37
35.	Isegere		300	150	134	126	16	142	34

APPENDIX B
RECORDED DATA FOR 11 KV OKESA FEEDER AT SUBSTATION FOR PEAK LOAD

S/N	S/S Name	Rating (KVA)	Red Phase / (Amp)	Yellow phase / (Amp)	Blue phase / (Amp)	Neutral / (Amp)	Load current / (Amp)	% Loading
1.	Police station	300	244	254	246	15	253	61
2.	Palace	500	567	589	556	23	578	83
3.	Old garage	500	456	446	449	18	456	66
4.	Idolofin	300	438	409	398	36	427	53
5.	Oke ese	300	222	265	228	59	258	62
6.	SUBEB	300	160	212	200	85	219	53
7.	Dallimore	500	395	348	558	187	496	71
8.	Okeyinmi	300	200	250	195	70	238	57
9.	Okeila 3 (rose bud)	500	438	382	419	110	453	65
10.	Okeila(ibo church)	300	220	180	226	65	230	55
11.	Odo Orobo	300	290	233	269	95	296	71
12.	Housing corporation	500	400	360	380	90	410	59
13.	Ekiti 1	300	91	161	165	15	144	35
14.	Ekiti 2	300	108	131	99	32	123	30
15.	Fed housing 1	300	450	185	248	100	328	71
16.	Fed housing 2	500	530	474	460	108	524	75
17.	Fed housing 3	500	164	226	272	111	264	38
18.	Fed housing phase 2	300	90	156	151	12	136	33
19.	Onala	300	212	169	218	60	220	53
20.	Park view 1	315	375	260	205	60	300	69
21.	Park view2	500	425	262	276	193	385	55
22.	Upper land	300	92	262	176	49	193	46
23.	Covenant	200	266	83	227	44	207	74
24.	Shelter view	500	180	77	251	47	185	27
25.	Prison	300	84	62	83	21	83	20